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(54) **APPARATUS FOR RADIATING LIGHT
FROM A VIRTUAL SOURCE**

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F21S 8/10 (2006.01)

(52) **U.S. Cl.**
CPC **F21S 48/1225** (2013.01); **F21S 48/115**
(2013.01); **F21S 48/1317** (2013.01); **F21S**
48/2212 (2013.01); **F21S 48/24** (2013.01)

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F21S 48/1159; F21S 48/2212
USPC 362/311.02, 311.09
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

7,153,002 B2 12/2006 Kim et al.
7,207,700 B2 4/2007 Fallahi et al.
7,401,948 B2 7/2008 Chinniah et al.
7,465,075 B2 12/2008 Chinniah et al.
7,489,453 B2 2/2009 Chinniah et al.

7,520,650 B2 4/2009 Smith
7,703,950 B2 4/2010 Ewert et al.
7,942,559 B2 5/2011 Holder et al.
7,976,192 B2 * 7/2011 Chinniah F21V 5/046
362/249.02
8,297,799 B2 * 10/2012 Chou F21K 9/135
359/725
8,979,320 B1 * 3/2015 McDermott G02B 19/0028
362/299
2004/0213001 A1 10/2004 Sayers et al.
2008/0304277 A1 12/2008 Chinniah et al.
2008/0310028 A1 12/2008 Chinniah et al.

OTHER PUBLICATIONS

SAE International. Printed Jan. 7, 2013. "Construction and Application of Near Field (TIR Type) lenses for Automotive Lighting Functions." <http://papers.sae.org/2007-01-1040/>.
Joo et al., LED beam shaping lens based on the near-field illumination, Optics Express, Dec. 7, 2009, pp. 23449-23458, vol. 17, No. 26, Optical Society of America.

* cited by examiner

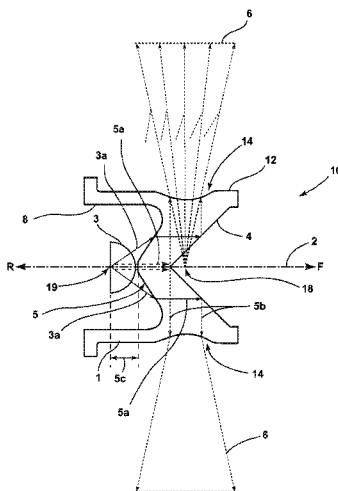
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(57) **ABSTRACT**

A lighting assembly that includes an LED source that generates a light cone (solid angle); and a transparent near field lens having a front surface, a collimating surface, and an aspherical groove. The collimating surface collimates the light cone into a beam that reflects off of the front surface toward the aspherical groove, and the aspherical groove directs the beam away from the lens as an exit cone from a virtual focal point, positive virtual focal ring or a negative virtual focal ring. The exit cone may be evenly distributed, substantially forward or substantially rearward from the virtual focal point or virtual focal ring. Parabolic or aspherical reflectors can be employed with lighting assemblies having a virtual focal point or virtual focal ring, respectively, to reflect the exit cone in a vehicular exterior lighting pattern.

7 Claims, 10 Drawing Sheets



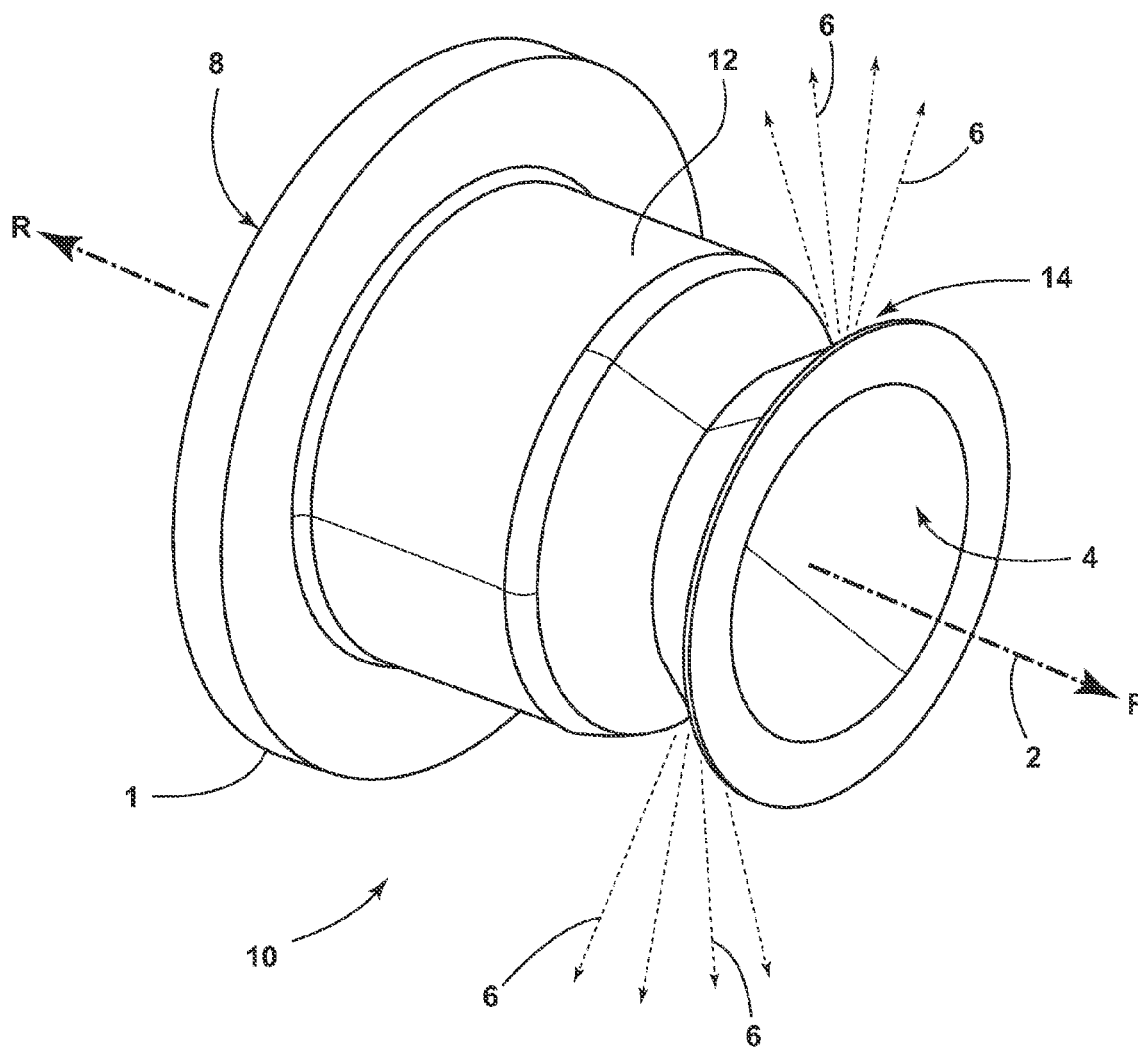


FIG. 1

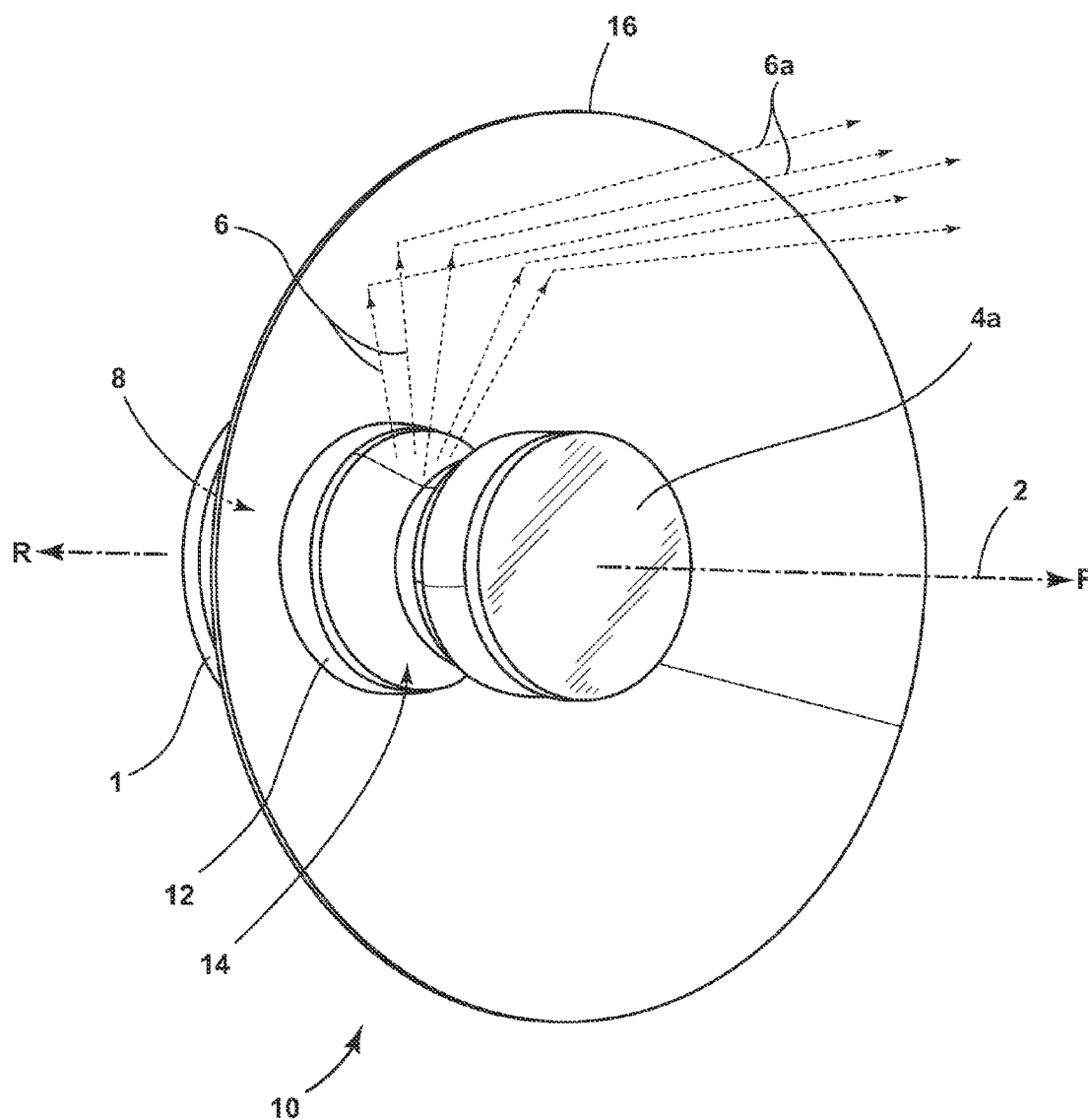


FIG. 2

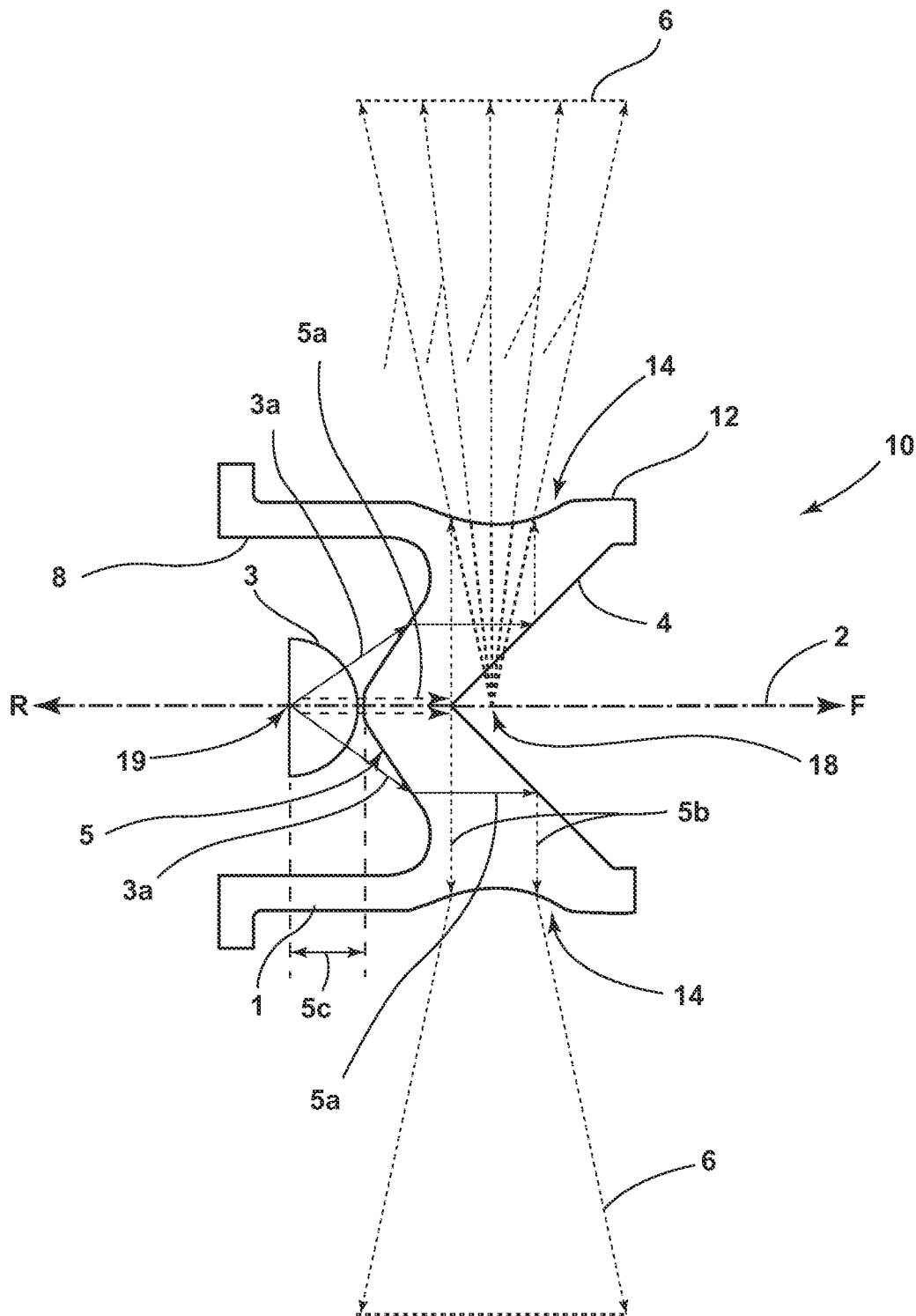


FIG. 3

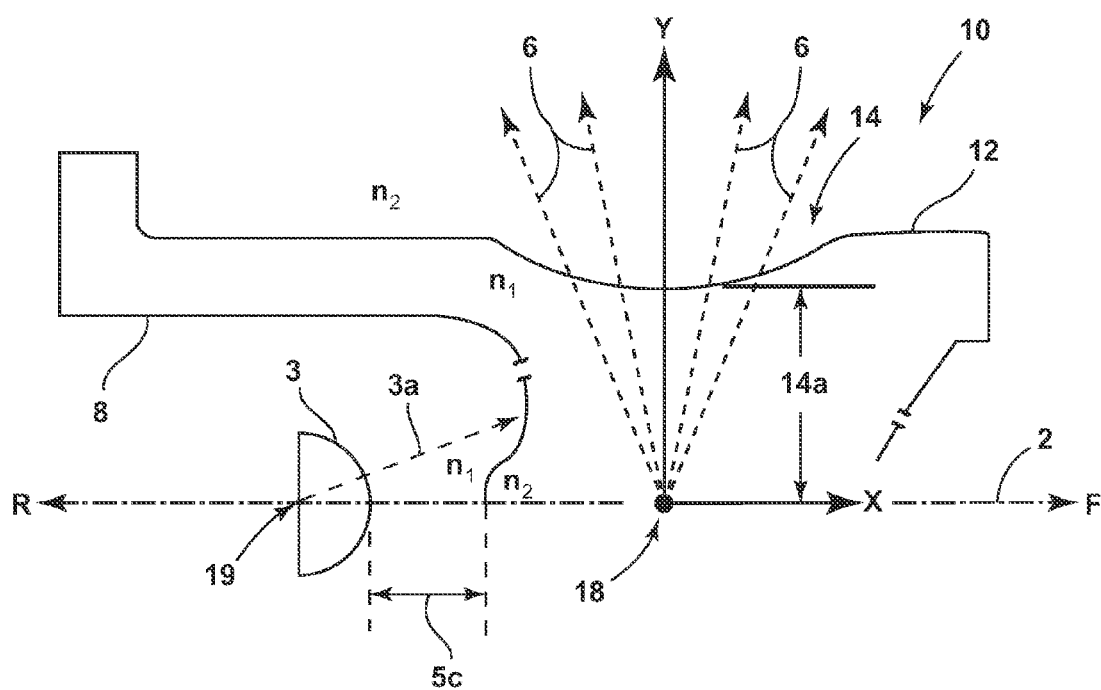


FIG. 3A

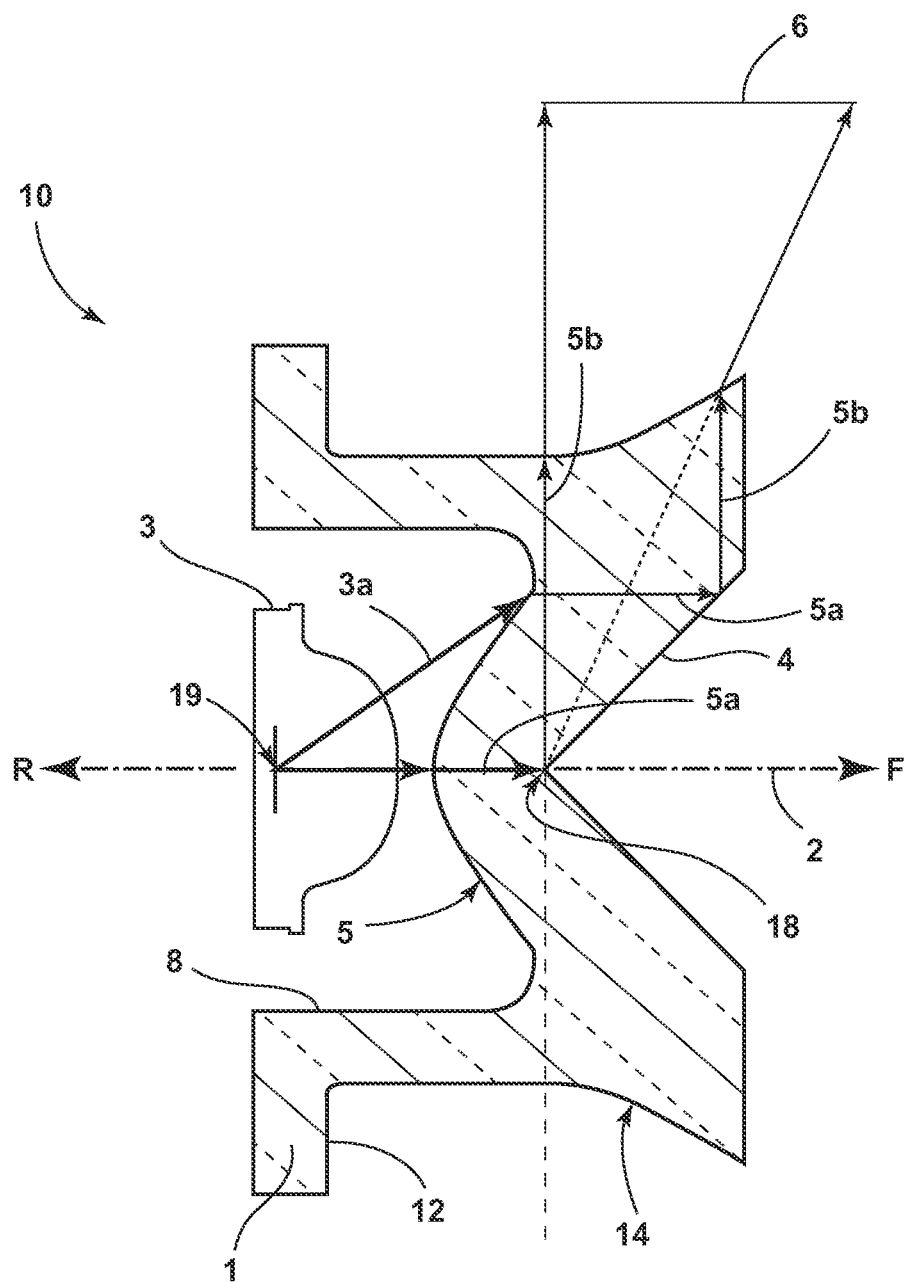


FIG. 4A

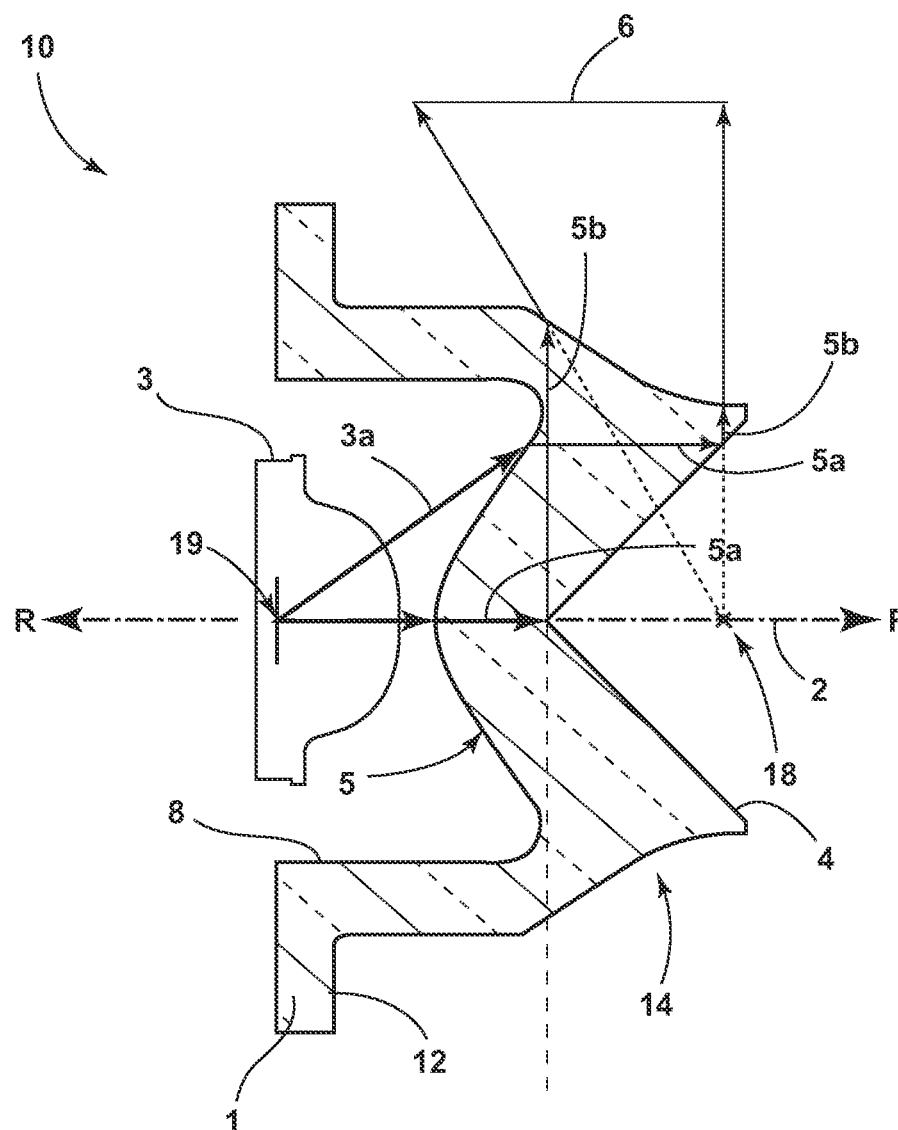


FIG. 4B

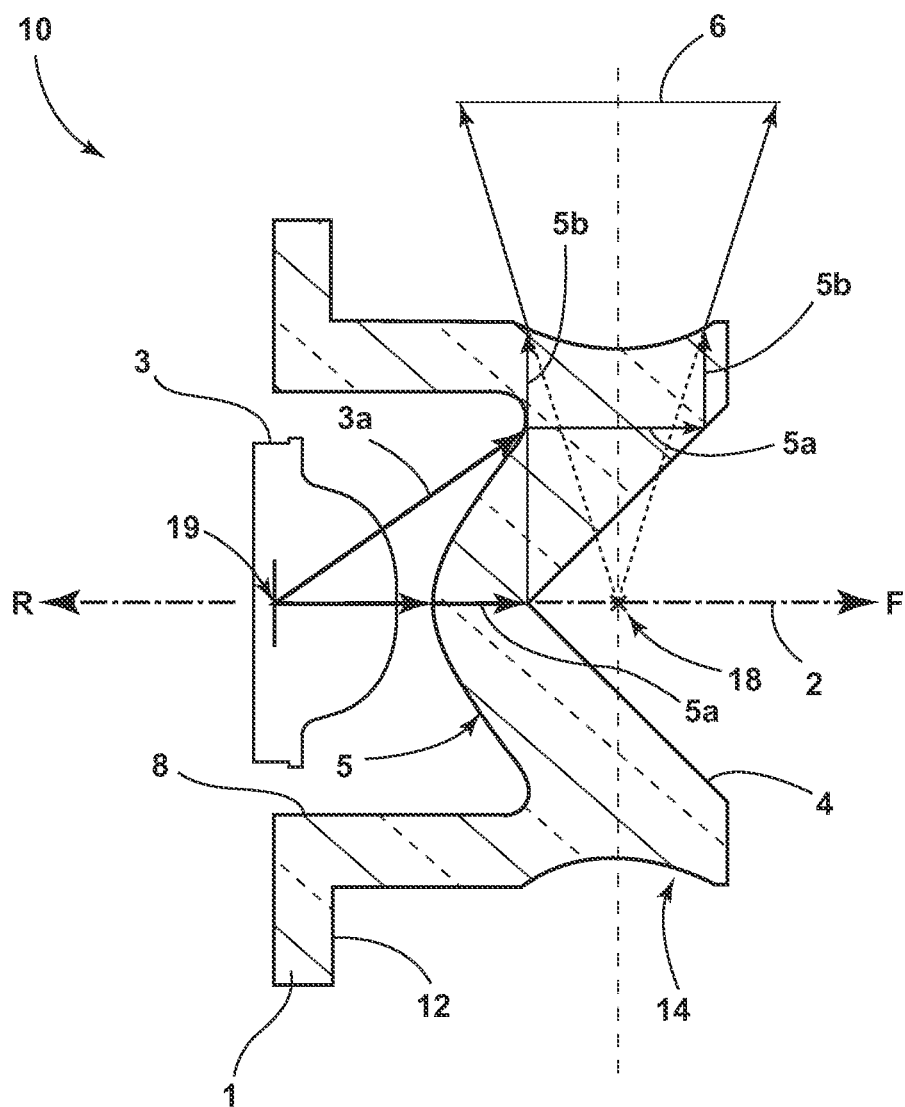


FIG. 4C

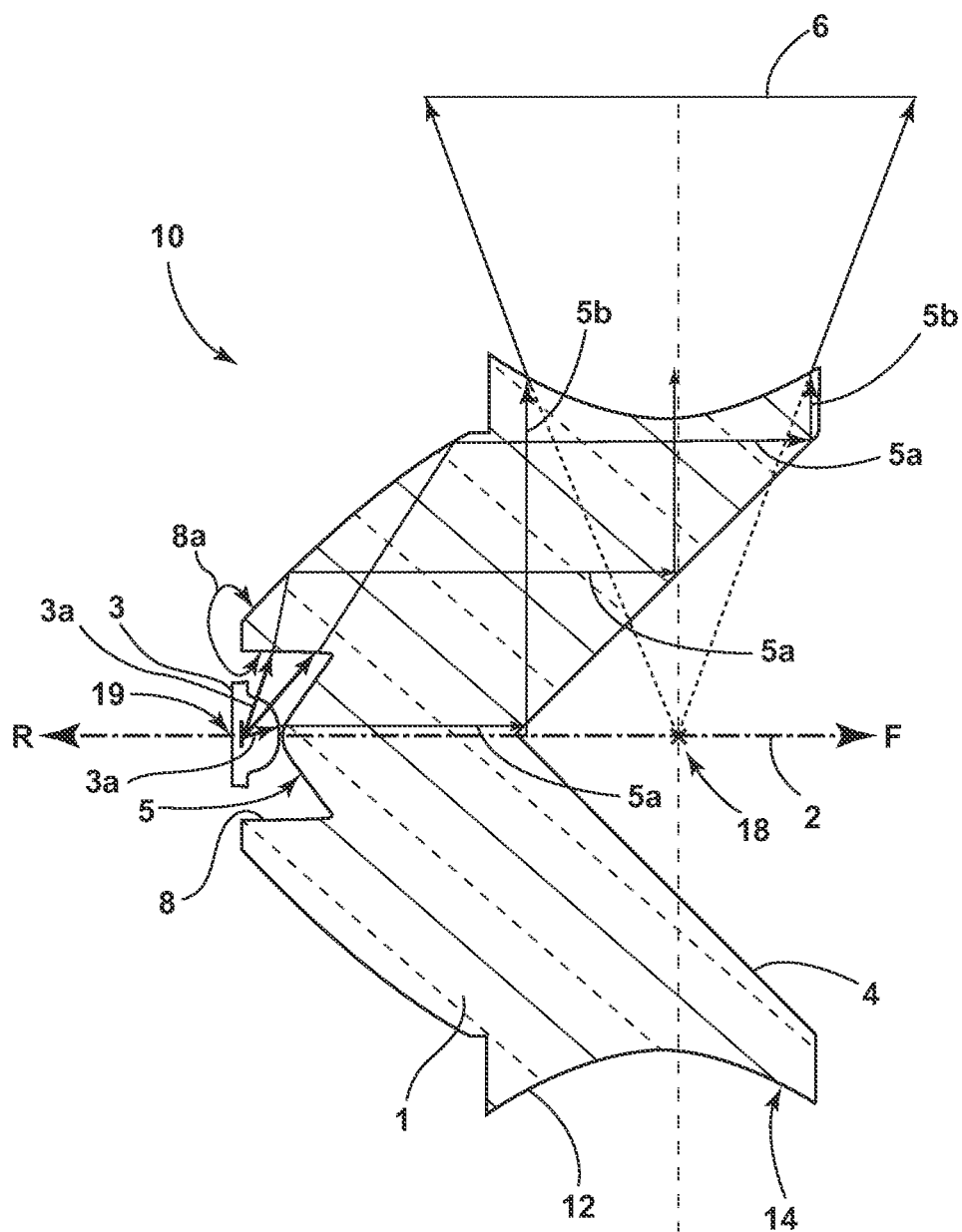


FIG. 4D

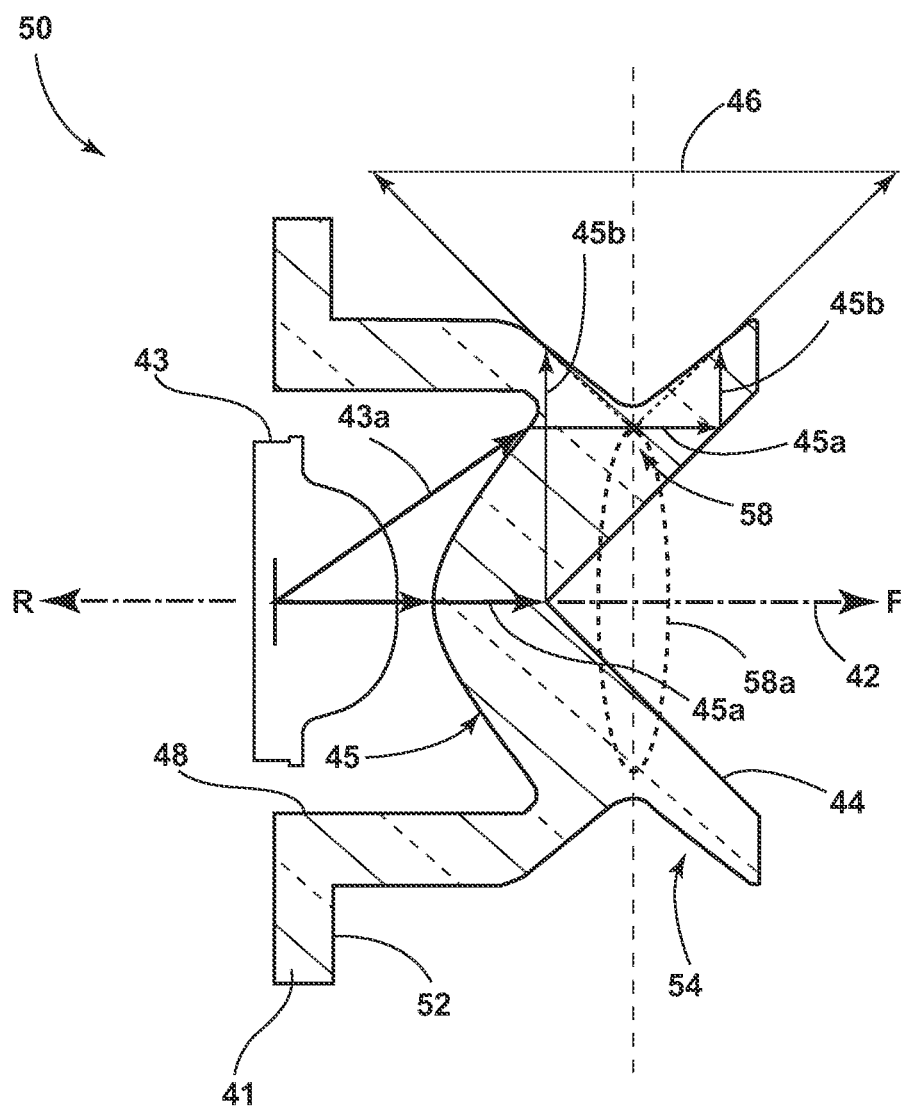


FIG. 5

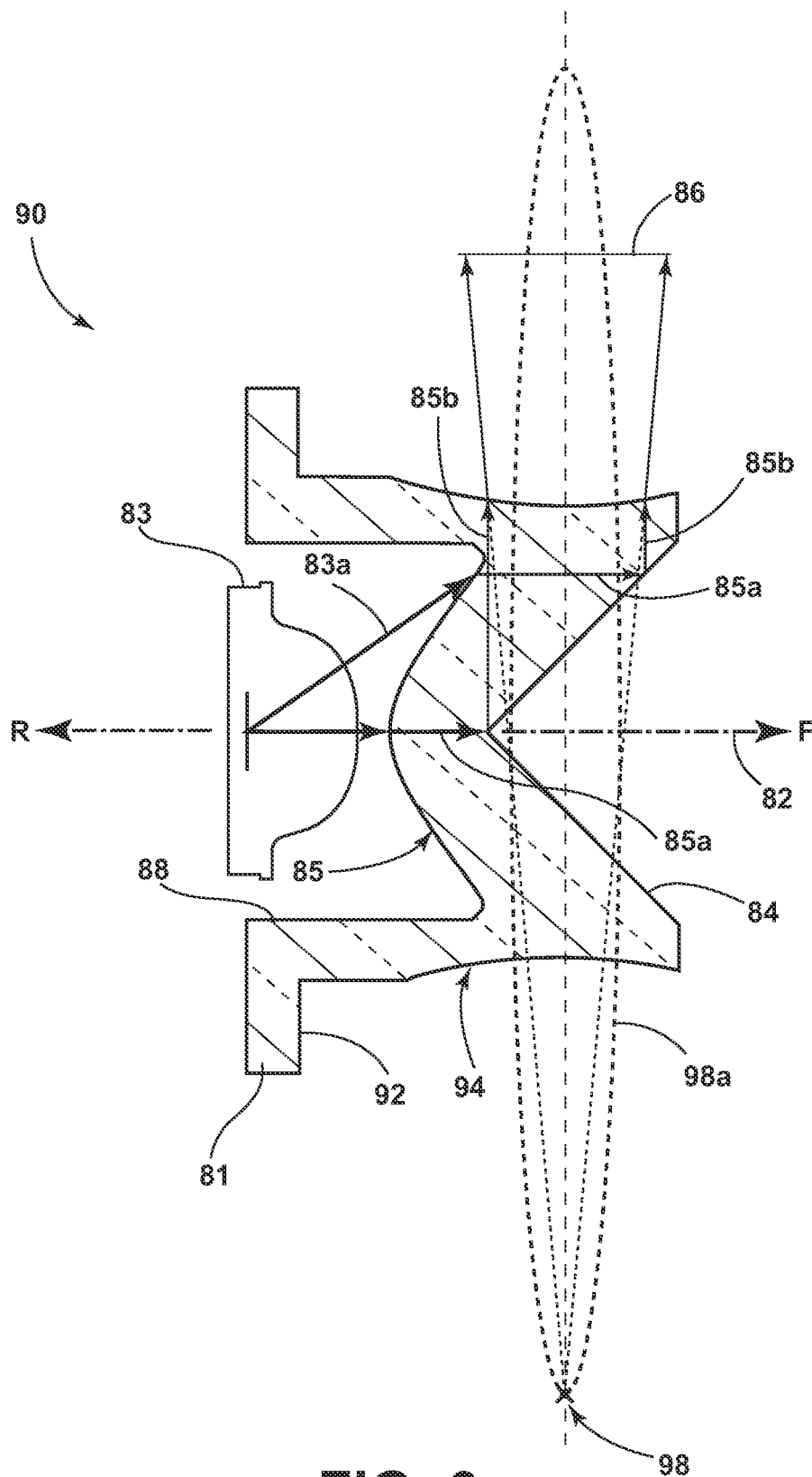


FIG. 6

1

APPARATUS FOR RADIATING LIGHT FROM A VIRTUAL SOURCE

FIELD OF THE INVENTION

The present invention generally relates to lighting assemblies, particularly LED-based lighting assemblies for use in vehicular lighting applications.

BACKGROUND OF THE INVENTION

Automotive lighting is significantly regulated by the federal government. Emitted light patterns, particularly those used in exterior lighting applications, must be controlled to meet federal regulations. The regulations exist to ensure the safety of drivers, pedestrians and other drivers in the environment of the vehicle. LED source technologies are rapidly becoming an efficient alternative to incandescent light bulb technologies. However, LED sources have a significant drawback in that they produce highly directional light. The directional nature of the light produced by LED sources has inhibited the development of LED-based lighting assemblies that can meet federal regulations, particularly in vehicular exterior lighting applications.

An LED source significantly differs from an incandescent light source in the form of the light it produces. Whereas light emanates from an incandescent light bulb in nearly 360°, light is emitted from an LED from one surface in the form of a cone (solid angle). Near-field lenses (NFLs) are used today to collimate the cone (solid angle) of light generated by an LED, but do little to increase the spread of light comparable to that produced by an incandescent bulb. Further, LED-based light that is collimated by a conventional NFL does not possess a focal point, usually a prerequisite for engineering other components, such as reflectors, that can also be employed in vehicular exterior lighting applications.

Accordingly, there is a need for an LED-based lighting assembly that can substantially replicate the light spread of an incandescent bulb and facilitate various packaging for use in certain applications, particularly vehicular exterior lighting applications.

SUMMARY OF THE INVENTION

According to one aspect of the present invention, a lighting assembly is provided. The lighting assembly includes an LED source that generates a light cone; and a transparent near field lens having a front surface, a collimating surface, and an aspherical groove. The collimating surface collimates the light cone into a beam that reflects off of the front surface toward the aspherical groove, and the aspherical groove directs the beam away from the lens as an exit cone from a virtual focal point.

According to another aspect of the present invention, a lighting assembly is provided. The lighting assembly includes an LED source that generates a light cone; and a transparent near field lens having a front surface, a collimating surface, and an aspherical groove. The collimating surface collimates the light cone into a beam that reflects off of the front surface toward the aspherical groove, and the aspherical groove directs the beam away from the lens as an exit cone from a positive virtual focal ring.

According to a further aspect of the present invention, a lighting assembly is provided. The lighting assembly includes an LED source that generates a light cone; and a transparent near field lens having a front surface, a collimating surface, and an aspherical groove. The collimating surface collimates the light cone into a beam that reflects off of the front surface toward the aspherical groove, and the aspherical groove directs the beam away from the lens as an exit cone from a negative virtual focal ring.

2

mating surface, and an aspherical groove. The collimating surface collimates the light cone into a beam that reflects off of the front surface toward the aspherical groove, and the aspherical groove directs the beam away from the lens as an exit cone from a negative virtual focal ring.

These and other aspects, objects, and features of the present invention will be understood and appreciated by those skilled in the art upon studying the following specification, claims, and appended drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

FIG. 1 is a perspective view of a lighting assembly with a near field lens having an aspherical groove according to one embodiment;

FIG. 2 is a perspective view of the lighting assembly depicted in FIG. 1 with a reflector according to another embodiment;

FIG. 3 is a schematic illustrating the operation of a lighting assembly with a near field lens having a collimating surface and an aspherical groove according to a further embodiment;

FIG. 3A is an enlarged view of the lighting assembly depicted in FIG. 3 demonstrating the development of the aspherical groove with an algorithm based on integral mathematics according to an additional embodiment;

FIG. 4A is a cross-sectional view of a lighting assembly with a near field lens having a collimating surface and an aspherical groove configured to direct an exit light cone from a virtual focal point in a substantially forward collective direction relative to the virtual focal point according to a further embodiment;

FIG. 4B is a cross-sectional view of a lighting assembly with a near field lens having a collimating surface and an aspherical groove configured to direct an exit light cone from a virtual focal point in a substantially rearward collective direction relative to the virtual focal point according to another embodiment;

FIG. 4C is a cross-sectional view of a lighting assembly with a near field lens having a collimating surface and an aspherical groove configured to direct an exit light cone from a virtual focal point in a collective direction that is substantially evenly distributed in the forward and rearward directions relative to the virtual focal point according to a further embodiment;

FIG. 4D is a cross-sectional view of a lighting assembly with a near field lens having a plurality of collimating surfaces and an aspherical groove configured to direct an exit light cone from a virtual focal point in a collective direction that is substantially evenly distributed in the forward and rearward directions relative to the virtual focal point according to another embodiment;

FIG. 5 is a cross-sectional view of a lighting assembly with a near field lens having a collimating surface and an aspherical groove configured to direct an exit light cone from a positive virtual focal ring according to an additional embodiment; and

FIG. 6 is a cross-sectional view of a lighting assembly with a near field lens having a collimating surface and an aspherical groove configured to direct an exit light cone from a negative virtual focal ring according to another embodiment.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

As required, detailed embodiments of the present invention are disclosed herein; however, it is to be understood that

3

the disclosed embodiments are merely exemplary of the invention that may be embodied in various and alternative forms. The figures are not necessarily to a detailed design; some schematics may be exaggerated or minimized to show function overview. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a representative basis for teaching one with ordinary skill in the art to variously employ the present invention.

For purposes of description herein, the terms “forward,” “rearward,” “side,” and derivatives thereof shall relate to the lighting assembly and components illustrated in FIG. 1. The “F” and “R” in FIG. 1 refer to forward and rearward directions, respectively. However, it is to be understood that the invention may assume various alternative orientations, except where expressly specified to the contrary. It is also to be understood that the specific devices and processes illustrated in the attached drawings, and described in the following specification are simply exemplary embodiments of the inventive concepts defined in the appended claims. Hence, specific dimensions and other physical characteristics relating to the embodiments disclosed herein are not to be considered as limiting, unless the claims expressly state otherwise.

Referring to FIG. 1, a perspective view of a lighting assembly 10 is depicted with a near field lens 1 having an aspherical groove 14 according to one embodiment. The near field lens 1 has a front surface 4 oriented in the forward direction “F,” and a rear surface 8 that faces an LED source (not shown in FIG. 1). As shown, the near field lens 1 is arranged symmetrically about an axis 2 that spans from the rearward direction “R” to the forward direction “F.” The near field lens 1 also possesses a side surface 12 configured around the axis 2 and defined between the front surface 4 and rear surface 8. The side surface 12 includes an aspherical groove 14.

The near field lens 1 is substantially transparent. Preferably, the near field lens element is constructed of glass, polycarbonate and/or polymethyl methacrylate (PMMA) materials. As readily understood by those with ordinary skill in the art, these materials should be sufficiently transparent for optical clarity. In general, an LED source 3 facing the rear surface 8 generates a light cone 3a (solid angle) (not shown) in the forward direction “F” that proceeds through the rear surface 8 into the near field lens 1 by way of refraction. The light from the light cone 3a (solid angle) is then substantially reflected within the lens 1 at the front surface 4 toward the side surface 12. A substantial portion of the reflected light from the light cone 3a (solid angle) then exits the lens 1 through the aspherical groove 14 as exit cone 6. Hence, the incident light from the LED source 3 in the form of light cone 3a (solid angle) is directed through the near field lens 1 and redirected out of lens 1 through the aspherical groove 14.

As defined herein, the term “aspherical” is associated with certain surfaces of the near field lens elements described in this disclosure. The “aspherical” surfaces of the near field lens elements described herein have a plurality of exterior points with different radius of curvature values. As such, these surfaces are “aspherical” in the sense that they cannot be extended and enclosed to form a perfect sphere.

As shown in FIG. 2, the lighting assembly 10 depicted in FIG. 1 can be configured with a reflector 16 according to another embodiment. The reflector 16 is configured about the axis 2 and around the side surface 12 of the near field lens 1. Further, the reflector 16 is located on the axis 2 at point rearward of the aspherical groove 14. Further, the

4

reflector 16 possesses an optically reflective exterior surface facing the forward direction “F” that is fabricated from reflective materials, as understood by those with ordinary skill in this art.

In the configuration depicted in FIG. 2, the lighting assembly 10 can harness the exit cone 6 from the lens 1 and redirect this light off of the reflector 16 in the forward direction “F.” The reflected light from the exit cone 6 now emanates in the forward direction “F” in the form of a light pattern 6a. Preferably, the near field lens 1 and the reflector 16 are engineered to create a light pattern 6a in a pattern with intensity and an angular spread that is suitable for vehicular exterior lighting applications that meet the operative federal regulations.

Referring again to FIG. 2, the near field lens 1 of lighting assembly 10 is depicted with a front surface cap 4a. As the light cone 3a (solid angle) emanating from LED source 3 and travelling through lens 1 is generally internally reflected off of front surface 4 (not shown), surface 4 can be covered by the front surface cap 4a. The cap 4a can be arranged as a stylistic element associated with the lighting assembly 10. Further, in some embodiments, cap 4a can possess a substantially reflective interior surface that faces front surface 4 of the near field lens 1 (not shown). The reflective interior surface of cap 4a can then reflect any light from the light cone 3a (solid angle) that is not reflected internally off of front surface 4 within the lens 1. Incorporating the reflective interior surface associated with cap 4a can thus improve the light collection efficiency of the lighting assembly 10.

In depicting a cross-section of lighting assembly 10, FIG. 3 demonstrates the operation of lighting assembly 10 according to another embodiment. As shown, the lighting assembly 10 includes an LED source 3 and a transparent near field lens 1. The LED source 3 generates a light cone 3a (solid angle). Preferably, the LED source 3 is arranged in proximity to the rear surface 8 of the lens 1 such that light cone 3a (solid angle) substantially impinges on the rear surface 8. LED source 3 can comprise one or more of various LED-related lighting sources that can provide a high intensity, directional light pattern in the form of a light cone 3a (solid angle). Other components (not shown) can be configured to power and control the LED source 3 as understood by those with ordinary skill in the art.

The near field lens 1 of the lighting assembly 10 depicted in FIG. 3 has a front surface 4 oriented in the forward direction “F,” and a rear surface 8 that faces the LED source 3. As shown, the near field lens 1 is arranged symmetrically about an axis 2 that spans from the rearward direction “R” to the forward direction “F.” The rear surface 8 further comprises a collimating surface 5. Note that in some embodiments, the rear surface 8 may comprise multiple collimating surfaces (see, e.g., collimating surfaces 5 and 8a shown in FIG. 4D). Further, as shown in FIG. 3, the near field lens 1 also possesses a side surface 12 configured around the axis 2 and defined between the front surface 4 and rear surface 8. The side surface 12 includes an aspherical groove 14.

Referring to FIG. 3 again, the near field lens 1 of lighting assembly 10 operates as follows. The LED source 3 facing the rear surface 8 generates a light cone 3a (solid angle) in the forward direction “F” that proceeds through the collimating surface 5 into the near field lens 1. Preferably, the collimating surface 5 is dimensionally configured to substantially collimate the cone 3a (solid angle) emanating from LED source 3. As such, collimating surface 5 can be larger or smaller depending upon the degree of spread associated with the light cone 3a (solid angle) emanating from the

5

particular LED source **3** employed in the lighting assembly **10**. Further, collimating surface **5** can be sized based on the relative location of LED source **3** in proximity to the collimating surface **5**. Preferably, collimating surface **5** is configured with a continuously varying radius of curvature.

The light from the light cone **3a** (solid angle) is then collimated by collimating surface **5** into a beam pattern **5a** within the near field lens **1** toward the front surface **4**. The beam pattern **5a** is then reflected within the lens **1** at the front surface **4** toward the side surface **12**. Front surface **4** is preferably configured at a roughly 45° angle within near field lens **1** to ensure complete internal reflection of the beam pattern **5a** toward the side surface **12**. As such, the beam pattern **5a** is reflected off of front surface **4** as reflected, cylindrical pattern **5b**.

A substantial portion of the reflected cylindrical pattern **5b** (originating from the light cone **3a** (solid angle)) then exits the near field lens **1** through the aspherical groove **14** of side surface **12** as exit cone **6**. In particular, the aspherical groove **14** directs the cylindrical pattern **5b** away from the lens **1** as an exit cone **6** with a virtual focal point **18** via refraction according to Snell's law. Although the exit cone **6** does not pass through virtual focal point **18**, its light rays can be traced back to virtual focal point **18**. The aspherical groove **14** is particularly engineered to spread the cylindrical pattern **5b** as an exit cone **6** in a direction corresponding to virtual focal point **18**. The aspherical groove **14** is also engineered to ensure that the critical angle associated with the refractive index of the material selected for near field lens **1** is not violated. When viewed in three dimensions, the lighting assembly **10** produces an exit cone **6** in the shape of a cylinder (with angular faces on the rearward side "R" and the forward side "F") with light emanating radially away from axis **2**. Preferably, aspherical groove **14** is engineered with a continuously varying radius of curvature.

As depicted in FIG. 3A, the aspherical groove **14** can be created using an algorithm, such as given below by Equation (1), based on integral mathematics. The aspherical groove **14** can be engineered in terms of its shape based on a desired location for virtual focal point **18** and the desired distance between virtual focal point **18** and the aspherical groove **14**. In particular, the aspherical groove **14** can be created in two dimensions in the X and Y coordinates as shown. The X coordinate is along the axis **2**, spanning from the rearward and forward directions, "R" and "F," respectively. The Y coordinate is normal to the X coordinate. The distance between the virtual focal point **18** (as-selected) and the bottommost point of the aspherical groove **14** toward the axis **2** is defined by focal length **14a**, also identified as "lf" in Equation (1) below. Further, n_1 and n_2 in Equation (1), and as depicted in FIG. 3A, correspond to the refractive index values of the near field lens **1** and environment surrounding the lens **1**, respectively.

As also depicted in FIG. 3A, the near field lens **1** will be surrounded by air and therefore n_2 will equal 1.00029 or 1 to simplify the equation. As noted earlier, lens **1** can be fabricated from a transparent material. In this example, lens **1** is fabricated of polycarbonate, giving it a refractive index, n_1 , equal to 1.586. Equation (1) can be employed to generate the curvature associated with aspherical groove **14**. For example, when the focal length **14a**, lf, is set at 10 mm, $f(x)=11.7411$ mm at $x=5$ mm. Ultimately, the aspherical groove **14** is defined according to Equation (1) such that $f(x)$ defines the location of the aspherical groove **14** along the Y axis as a function of location along the X axis.

6

$$f(x) = \sqrt{\left(\left(\frac{\left(\frac{lf}{\left(\frac{n_1}{n_2} + 1 \right)} \right)^2}{\left(\frac{n_1}{n_2} - 1 \right)} \right) \times \left(\frac{x^2}{\left(\frac{\left(\frac{n_1}{n_2} + 1 \right)}{\left(\frac{n_1}{n_2} - 1 \right)} \right)} + 1 \right) \right)^2 + \left(\frac{\left(\frac{n_1}{n_2} \right) \times \left(\frac{lf}{\left(\frac{\left(\frac{n_1}{n_2} + 1 \right)}{\left(\frac{n_1}{n_2} - 1 \right)} \right)} \right)}{\left(\frac{n_1}{n_2} - 1 \right)} \right)^2} \quad (1)$$

Referring to FIGS. 3 and 3A, it should also be understood that aspherical collimating surface **5** can be created using an algorithm based on integral mathematics that is similar to Equation (1). In particular, Equation (2) below can be employed to generate the curvature associated with the collimating surface **5**. In this example, n_1 will represent air with a refractive index of 1.00029 or 1 (to simplify the equation) and n_2 will represent the transparent material polycarbonate with a refractive index of 1.586. The X and Y directions employed in Equation (2) relative to the collimating surface **5** shown in FIGS. 3 and 3A are shifted 90 degrees relative to those employed in Equation (1) for aspherical groove **14**. Further, the lf term in the Equation (2) corresponds to the focal length **5c** for the collimating surface **5**, defined by the distance in the axis **2** direction between the LED focal point **19** and the center point of the collimating surface **5** (not shown in FIG. 3). As such, $f(x)$ in Equation (2) can be used to define the collimating surface **5** in the axis **2** direction (along the axis formed by the "R" and "F" directions) as a function of the X direction, defined normal to the axis **2**. It should be understood that there are many ways to create a collimated beam through collimating surface **5** into near field lens **1**, whether by a single or multiple surfaces. Hence, the algorithms employed in Equation (2) are merely exemplary.

$$f(x) = \sqrt{\left(\left(\frac{\left(\frac{lf}{\left(\frac{n_2}{n_1} + 1 \right)} \right)^2}{\left(\frac{n_2}{n_1} - 1 \right)} \right) \times \left(\frac{x^2}{\left(\frac{\left(\frac{n_2}{n_1} + 1 \right)}{\left(\frac{n_2}{n_1} - 1 \right)} \right)} + 1 \right) \right)^2 + \left(\frac{\left(\frac{n_2}{n_1} \right) \times \left(\frac{lf}{\left(\frac{\left(\frac{n_2}{n_1} + 1 \right)}{\left(\frac{n_2}{n_1} - 1 \right)} \right)} \right)}{\left(\frac{n_2}{n_1} - 1 \right)} \right)^2} \quad (2)$$

7

Additional embodiments of lighting assembly 10 are depicted in FIGS. 4A-4C. In FIG. 4A, a cross-section of a lighting assembly 10 is depicted in which the near field lens 1 is configured to produce an exit cone 6 from a virtual focal point 18 in a substantially forward direction relative to the virtual focal point 18. As shown in FIG. 4A, the aspherical groove 14 is particularly engineered to refract cylindrical pattern 5b in a forward direction such that a substantial portion of light rays in exit cone 6 have a forward direction "F" component. All of the light rays that form exit cone 6 can be traced back in the direction of virtual focal point 18. Preferably, the virtual focal point 18 resides within or in proximity to near field lens 1 when the aspherical groove 14 is engineered to produce a substantially forward-oriented exit cone 6. Further, a reflector 16 can be engineered and fitted to the lighting assembly 10 of FIG. 4A to collect and reflect the exit cone 6 as a light pattern 6a (see FIG. 2). Preferably, the reflector 16 is configured as a parabolic reflector (e.g., a paraboloid shape) having a focal point consistent with virtual focal point 18.

In FIG. 4B, a cross-section of a lighting assembly 10 is depicted in which the near field lens 1 is configured to produce an exit cone 6 from a virtual focal point 18 in a substantially rearward direction relative to the virtual focal point 18. As shown in FIG. 4B, the aspherical groove 14 is particularly engineered to refract cylindrical pattern 5b in a rearward direction such that a substantial portion of light rays in exit cone 6 have a rearward direction "R" component. All of the light rays that form exit cone 6 can be traced back in the direction of virtual focal point 18. Preferably, the virtual focal point 18 resides forward of front surface 4 of near field lens 1 when the aspherical groove 14 is engineered to produce a substantially rearward-oriented exit cone 6. Further, a reflector 16 can be engineered and fitted to the lighting assembly 10 of FIG. 4B to collect and reflect the exit cone 6 as a light pattern 6a (see FIG. 2). Preferably, the reflector 16 is configured as a parabolic reflector (e.g., a paraboloid shape) having a focal point consistent with virtual focal point 18.

Referring to FIG. 4C, a cross-section of a lighting assembly 10 is depicted in which the near field lens 1 is configured to produce an exit cone 6 from a virtual focal point 18 in a collective direction that is substantially evenly distributed in the forward and rearward directions "F" and "R" relative to the virtual focal point 18. As shown in FIG. 4C, the aspherical groove 14 is particularly engineered to refract cylindrical pattern 5b in a substantially uniform fashion such that roughly equivalent portions of the light rays in exit cone 6 have a rearward direction "R" component or a forward direction "F" component, respectively. All of the light rays that form exit cone 6 can be traced back in the direction of virtual focal point 18. Preferably, the virtual focal point 18 resides centrally located to cylindrical pattern 5b of near field lens 1. Further, a reflector 16 can be engineered and fitted to the lighting assembly 10 of FIG. 4C to collect and reflect the exit cone 6 as a light pattern 6a (see FIG. 2). Preferably, the reflector 16 is configured as a parabolic reflector (e.g., a paraboloid shape) having a focal point consistent with virtual focal point 18.

Referring to FIG. 4D, a cross-section of a lighting assembly 10 is depicted in which the near field lens 1 is configured with multiple collimating surfaces, collimating surface 5 and collimating surfaces 8a, to produce an exit cone 6 from a virtual focal point 18 in a collective direction that is substantially evenly distributed in the forward and rearward directions "F" and "R" relative to the virtual focal point 18. In particular, the LED source 3 facing the rear surface 8

8

generates a light cone 3a (solid angle) in the forward direction "F" that proceeds through the collimating surface 5 and collimating surface 8a, into the near field lens 1. Further, the interior side of collimating surface 8a also collimates some of the light that has refracted through another region of collimating surface 8a. Preferably, the collimating surfaces 5 and 8a are dimensionally configured to substantially collimate the cone 3a (solid angle) emanating from LED source 3. As such, collimating surfaces 5 and 8a can be larger or smaller depending upon the degree of spread associated with the light cone 3a (solid angle) emanating from the particular LED source 3 employed in the lighting assembly 10. Further, collimating surfaces 5 and 8a can be sized based on the relative location of LED source 3 in proximity to the collimating surfaces 5 and 8a.

The light from the light cone 3a (solid angle) is then collimated by collimating surfaces 5 and 8a into a beam pattern 5a within the near field lens 1 toward the front surface 4. The beam pattern 5a is then reflected within the lens 1 at the front surface 4 toward the side surface 12. Front surface 4 is preferably configured at a roughly 45° angle within near field lens 1 to ensure complete internal reflection of the beam pattern 5a toward the side surface 12. As such, the beam pattern 5a is reflected off of front surface 4 as reflected, cylindrical pattern 5b.

As further shown in FIG. 4D, the aspherical groove 14 is particularly engineered to refract cylindrical pattern 5b in a substantially uniform fashion such that roughly equivalent portions of the light rays in exit cone 6 have a rearward direction "R" component or a forward direction "F" component, respectively. All of the light rays that form exit cone 6 can be traced back in the direction of virtual focal point 18. Preferably, the virtual focal point 18 resides centrally located to cylindrical pattern 5b of near field lens 1. Further, a reflector 16 can be engineered and fitted to the lighting assembly 10 of FIG. 4D to collect and reflect the exit cone 6 as a light pattern 6a (see FIG. 2). Preferably, the reflector 16 is configured as a parabolic reflector (e.g., a paraboloid shape) having a focal point consistent with virtual focal point 18.

Referring to FIG. 5, a lighting assembly 50 is depicted according to another embodiment in a cross-sectional view. Notably, lighting assembly 50 possesses a near field lens 41 having a collimating surface 45 and an aspherical groove 54 configured to direct an exit light cone 46 from a positive virtual focal ring 58a. Equations (1) and (2) can be employed to create the aspherical groove 54 and collimating surface 45, respectively. As shown, the lighting assembly 50 includes an LED source 43 and a transparent near field lens 41. The LED source 43 generates a light cone 43a (solid angle). It is preferable for the LED source 43 to be arranged in proximity to the rear surface 48 of the lens 41 such that light cone 43a (solid angle) substantially impinges on the rear surface 48. LED source 43 can comprise one or more of various LED-related lighting sources that can provide a high intensity, directional light pattern in the form of a light cone 43a (solid angle). As understood by those with ordinary skill, other components (not shown) can be configured to power and control the LED source 43.

The near field lens 41 of the lighting assembly 50 depicted in FIG. 5 has a front surface 44 oriented in the forward direction "F," and a rear surface 48 that faces the LED source 43. As shown, the near field lens 41 is arranged symmetrically about an axis 42 that spans from the rearward direction "R" to the forward direction "F". The rear surface 48 further comprises a collimating surface 45. In addition, the near field lens 41 also possesses a side surface 52

configured around the axis 42 and defined between the front surface 44 and rear surface 48. The side surface 52 includes an aspherical groove 54.

Referring to FIG. 5 again, the near field lens 41 of lighting assembly 50 operates as follows. The LED source 43 facing the rear surface 48 generates a light cone 43a (solid angle) in the forward direction “F” that proceeds through the collimating surface 45 into the near field lens 41. Preferably, the collimating surface 45 is dimensionally configured to substantially collimate the light cone 43a (solid angle) emanating from LED source 43. Collimating surface 45 can therefore be larger or smaller depending upon the degree of spread associated with the light cone 43a (solid angle) emanating from the particular LED source 43 employed in the lighting assembly 50. In addition, collimating surface 45 can be sized based on its location in proximity to the location of LED source 43.

The light from the light cone 43a (solid angle) is then collimated by collimating surface 45 into a beam pattern 45a within the near field lens 41 toward the front surface 44 in the forward direction “F.” The beam pattern 45a is then reflected within the lens 41 at the front surface 44 toward the side surface 52. Front surface 44 is preferably configured at a roughly 45° angle within near field lens 41 to ensure complete internal reflection of the beam pattern 45a toward the side surface 52. As such, the beam pattern 45a is reflected off of front surface 44 as reflected cylindrical pattern 45b.

A substantial portion of the reflected cylindrical pattern 45b (originating from the light cone 43a (solid angle)) then exits the near field lens 41 through the aspherical groove 54 of side surface 52 as exit cone 46. In particular, the aspherical groove 54 directs the cylindrical pattern 45b away from the lens 41 as an exit cone 46 with a virtual focal point 58 via refraction according to Snell’s law. Although the exit cone 46 does not pass through virtual focal point 58, its light rays can be traced back to virtual focal point 58. In particular, the aspherical groove 54 is engineered to spread the cylindrical pattern 45b as an exit cone 46 in a direction corresponding to virtual focal point 58. The aspherical groove 54 is also engineered to ensure that the critical angle associated with the refractive index of the material selected for near field lens 41 is not violated.

Further, the virtual focal point 58 is situated above the axis 42 and aspherical groove 54. As a consequence, each cross-sectional view of lighting assembly 50 and near field lens 41 will depict a virtual focal point 58 at a different location in space. Together, these virtual focal points 58 trace a positive virtual focal ring 58a, denoted in perspective as a dotted ellipse in FIG. 5. Hence, a plurality of exit cones 46 emanate from the positive virtual focal ring 58a when lighting assembly 50 is viewed in perspective in three dimensions.

Referring further to FIG. 5, the exit cone 46 of lighting assembly 50 is in the shape of a cylinder (with angular faces on the rearward side “R” and the forward side “F”) with light emanating radially away from axis 42 when the cone 46 is viewed in three dimensions. Preferably, aspherical groove 54 is engineered with a continuously varying radius of curvature to produce virtual focal points 58 and positive virtual focal ring 58a. It should also be understood that the exit cone 46 associated with lighting assembly 50 with a positive virtual focal ring 58a possesses a large angular spread, preferably greater than 45°. As such, the cylindrical shape of exit cone 46 (as viewed in three dimensions) is a cylinder with a large height dimension along the axis 42. It should be understood that the techniques for shifting the exit

cone 6 in the lighting assemblies 10 depicted in FIGS. 4A and 4B can also be applied to shift the exit cone 46 of lighting assembly 50 depicted in FIG. 5.

Further, a reflector 16 (see FIG. 2) can be engineered and fitted to the lighting assembly 50 of FIG. 5 to collect and reflect the exit cone 46 as a light pattern directed substantially in the forward direction “F” (not shown). Preferably, the reflector 16 employed in connection with lighting assembly 50 is configured as an asparabolic reflector (e.g., a substantially paraboloid-like shape using a parabolic curve built from a virtual focal point and revolved around the central axis 42) having a plurality of focal points consistent with the virtual focal ring 58a. Given the relatively large angular spread of the exit cone 46, the reflector 16 must be sufficiently large to reflect all of the light from exit cone 46. A light pattern with a large angular spread generated by a lighting assembly 50 could be employed in certain vehicular exterior lighting applications, to support such functions as daytime running lamp (DRL), stop, turn, etc.

Referring to FIG. 6, a lighting assembly 90 is depicted according to an additional embodiment in a cross-sectional view. Lighting assembly 90 possesses a near field lens 81 having a collimating surface 85 and an aspherical groove 94 configured to direct an exit light cone 86 from a negative virtual focal ring 98a. Equations (1) and (2) can be employed to create the aspherical groove 94 and collimating surface 85, respectively. As shown, the lighting assembly 90 includes an LED source 83 and a transparent near field lens 81. The LED source 83 generates a light cone 83a (solid angle). Preferably, the LED source 83 is arranged in proximity to the rear surface 88 of the lens 81 such that light cone 83a (solid angle) substantially impinges on the rear surface 88. LED source 83 can comprise one or more of various LED-related lighting sources that can provide a high intensity, directional light pattern in the form of a light cone 83a (solid angle). As readily understood by those with ordinary skill, other components (not shown) can be configured to power and control the LED source 83.

The near field lens 81 of the lighting assembly 90 depicted in FIG. 6 has a front surface 84 oriented in the forward direction “F,” and a rear surface 88 that faces the LED source 83. As shown, the near field lens 81 is arranged symmetrically about an axis 82 that spans from the rearward direction “R” to the forward direction “F”. The rear surface 88 further comprises a collimating surface 85. In addition, the near field lens 81 also possesses a side surface 92 configured around the axis 82 and defined between the front surface 84 and rear surface 88. The side surface 92 includes an aspherical groove 94.

Referring again to FIG. 6, the near field lens 81 of lighting assembly 90 operates as follows. The LED source 83 facing the rear surface 88 generates a light cone 83a (solid angle) in the forward direction “F” that proceeds through the collimating surface 85 into the near field lens 81. Preferably, the collimating surface 85 is dimensionally configured to substantially collimate the cone 83a (solid angle) emanating from LED source 83. Collimating surface 85 can therefore be sized based upon the degree of spread associated with the light cone 83a (solid angle) emanating from the particular LED source 83 employed in the lighting assembly 90. In addition, the collimating surface 85 can be sized based on its location in proximity to the location of LED source 43.

The light from the light cone 83a (solid angle) is then collimated by collimating surface 85 into a beam pattern 85a within the near field lens 81 toward the front surface 84 in the forward direction “F”. The beam pattern 85a is then reflected within the lens 81 at the front surface 84 toward the

11

side surface **92**. Front surface **84** is preferably configured at a roughly 45° angle within near field lens **81** to ensure complete internal reflection of the beam pattern **85a** toward the side surface **92**. As such, the beam pattern **85a** is reflected off of front surface **84** as reflected cylindrical pattern **85b**.

A substantial portion of the cylindrical beam pattern **85b** (originating from the light cone **83a**) then exits the near field lens **81** through the aspherical groove **94** of side surface **92** as exit cone **86**. In particular, the aspherical groove **94** directs the cylindrical pattern **85b** away from the lens **81** as an exit cone **86** with a virtual focal point **98** via refraction according to Snell's law. Although the exit cone **86** does not pass through virtual focal point **98**, its light rays can be traced back to virtual focal point **98**. In particular, the aspherical groove **94** is engineered to spread the cylindrical pattern **85b** as an exit cone **86** in a direction corresponding to virtual focal point **98**. The aspherical groove **94** is also engineered to ensure that the critical angle associated with the refractive index of the material selected for near field lens **81** is not violated.

Further, the virtual focal point **98** is situated below the axis **82**, and outside of the near field lens **81** and aspherical groove **94**. As a consequence, each cross-sectional view of lighting assembly **90** and near field lens **81** will depict a virtual focal point **98** at a different location in space. Together, these virtual focal points **98** trace a negative virtual focal ring **98a**, denoted in perspective as a dotted ellipse in FIG. 6. Hence, a plurality of exit cones **86** emanate from the negative virtual focal ring **98a** when lighting assembly **90** is viewed in perspective in three dimensions.

Referring further to FIG. 6, the exit cone **86** of lighting assembly **90** is in the shape of a cylinder (with angular faces on the rearward side "R" and the forward side "F") with light emanating radially away from axis **82** when the cone **86** is viewed in three dimensions. Preferably, aspherical groove **94** is engineered with a continuously varying radius of curvature to produce virtual focal points **98** and negative virtual focal ring **98a**. It should also be understood that the exit cone **86** associated with lighting assembly **90** with a negative virtual focal ring **98a** possesses a small angular spread, typically less than 45°. As such, the cylindrical shape of exit cone **86** (as viewed in three dimensions) is a cylinder with a small height dimension along the axis **82**. It should be understood that the techniques for shifting the exit cone **6** in the lighting assemblies **10** depicted in FIGS. 4A and 4B can also be applied to shift the exit cone **86** of lighting assembly **90** depicted in FIG. 6.

Further, a reflector **16** (see FIG. 2) can be engineered and fitted to the lighting assembly **90** of FIG. 6 to collect and reflect the exit cone **86** as a light pattern directed substantially in the forward direction "F" (not shown). Preferably, the reflector **16** employed in connection with lighting assembly **90** is configured as an asparabolic reflector (e.g., a substantially paraboloid-like shape using a parabolic curve built from a virtual focal point and revolved around the central axis **82**) having a plurality of focal points consistent with the virtual focal ring **98a**. Given the relatively small angular spread of the exit cone **86**, the reflector **16** can be comparably packaged with small dimensions sufficient to reflect all of the light from exit cone **86**. The net effect is an advantageously narrow angular spread (compared to the broad pattern produced by lighting assembly **50**) in the forward direction "F," significantly larger in angular spread than the light cone **83a** (solid angle) that emanates from the LED source **83**. An intense light pattern with a relatively narrow angular spread generated by a lighting assembly **90**

12

could be employed in certain vehicular exterior lighting applications to support such functions as DRL, stop, turn, etc.

The lighting assembly embodiments described in the foregoing, including lighting assemblies **10**, **50** and **90**, advantageously harness the benefits of LED-based lighting sources (e.g., power consumption), while providing angular spreads typically associated with incandescent applications. Further, these lighting assemblies employ near field lenses with one or more collimating surface(s) and aspherical groove elements that advantageously utilize side-emitting NFL technology, but further provide the precise optical design control associated with virtual focal points and virtual focal rings. With known and precise virtual focal points and virtual focal rings, depending upon the type of lighting assembly employed, it is possible to engineer other exterior lighting components (e.g., reflectors) to more efficiently harness the light emanating from the NFLs associated with these lighting assemblies. One significant advantage associated with these engineered lighting assemblies is the ability to reduce the overall aspect ratio of the exterior lighting assembly, or otherwise optimize the packaging of the assembly, as compared to conventional incandescent lighting technologies.

It is to be understood that variations and modifications can be made on the aforementioned structure including, but not limited to, the collimation surface or surfaces, and associated algorithms, without departing from the concepts of the present invention, and further it is to be understood that such concepts are intended to be covered by the following claims unless these claims by their language expressly state otherwise.

What is claimed is:

1. A lighting assembly, comprising:

an LED source that generates a light cone; and
a transparent near field lens having a front surface, a collimating surface, and an aspherical groove,
wherein the collimating surface collimates the light cone into a beam that reflects off of the front surface toward the groove, the groove shaped to spread the beam as an exit cone substantially evenly distributed from a virtual focal point in forward and rearward directions.

2. The lighting assembly according to claim 1, wherein the near field lens is configured in proximity to the LED source such that the collimating surface collimates a substantial portion of the light cone into the beam that reflects off of the front surface toward the aspherical groove.

3. The lighting assembly according to claim 1, wherein the aspherical groove possesses a continuously varying radius of curvature.

4. A lighting assembly, comprising:

an LED source that generates a light cone; and
a transparent near field lens having a front surface, a plurality of collimating surfaces, and an aspherical groove,
wherein the collimating surfaces collimate the light cone into a beam that reflects off of the front surface toward the groove, the groove shaped to spread the beam as an exit cone substantially evenly distributed from a virtual focal point in forward and rearward directions.

5. The lighting assembly according to claim 4, wherein the near field lens is configured in proximity to the LED source such that the collimating surfaces collimate a substantial portion of the light cone into the beam that reflects off of the front surface toward the aspherical groove.

13

6. The lighting assembly according to claim 4, wherein the aspherical groove possesses a continuously varying radius of curvature.

7. The lighting assembly according to claim 4, further comprising:

a parabolic reflector configured to reflect the exit cone in a vehicular exterior lighting pattern.

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14

5